

Airfoil Shape Optimization Using Output-Based Adapted Meshes

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Outline

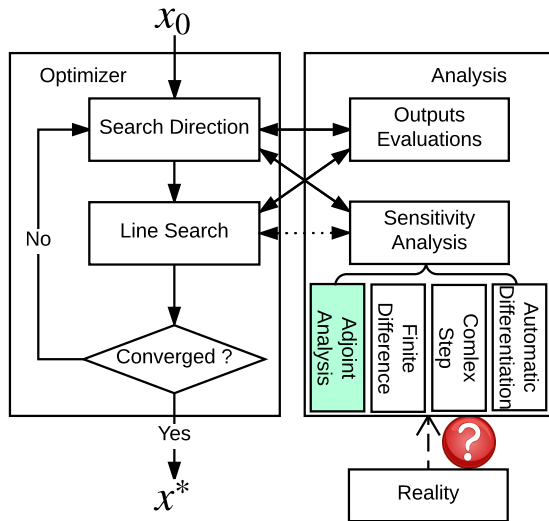
- 1 Introduction
- 2 Optimization Problem
- 3 Discretization
- 4 Error Estimation and Mesh Adaptation
- 5 Optimization Approach
- 6 Results and Discussion
- 7 Conclusions and Future Work



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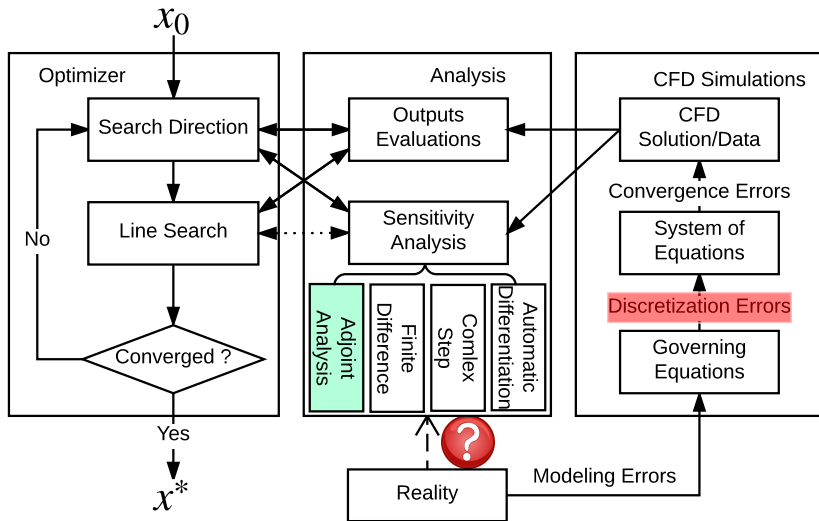
Aerodynamic Shape Design/Optimization

Design/Optimization: Numerical Optimization + CFD Analysis



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Improving Optimization Accuracy and Efficiency

Traditional methods

- a *a priori* mesh: numerical error not controlled during optimization
- fixed fidelity: optimizing on fixed mesh resolution

Proposed method

- Multi-fidelity optimization: reduce the computational resources at the early stages of optimization
- Adjoint based error estimation and mesh adaptation: actively control the numerical error during the optimization
- $\xrightarrow{\text{Integration}}$ Multi-fidelity optimization driven by error estimation and mesh adaptation:
Initial shape \Rightarrow Optimal design, Coarse mesh \Rightarrow Fine mesh
Goal: prevent over-refining and over-optimizing



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Optimization Problem Formulation

General optimization problem

- Determine the design variables \mathbf{x} that minimize the objective function J :

$$\begin{aligned} & \min_{\mathbf{x}} J(\mathbf{U}, \mathbf{x}) \\ \text{s.t. } & \mathbf{R}^e(\mathbf{U}, \mathbf{x}) = \mathbf{0} \\ & \mathbf{R}^{ie}(\mathbf{U}, \mathbf{x}) \geq \mathbf{0} \end{aligned}$$

- \mathbf{U} denotes the flow variables, \mathbf{R}^e and \mathbf{R}^{ie} are the equality and inequality constraints.

Aerodynamic optimization

- Objective and constraints are aerodynamic outputs
- Physical feasibility: Flow variables \mathbf{U} are solved within a feasible design space Ω to satisfy the flow equations,

$$\mathbf{R}(\mathbf{U}, \mathbf{x}) = \mathbf{0}, \quad \forall \mathbf{x} \in \Omega$$



Objective and trim constraints

- Objective outputs: directly targeted for mesh adaptation, denoted as J^{adapt}
- Trim constraints: We only consider the equality constraints \mathbf{R}^e and active inequality constraints \mathbf{R}_a^{ie} ,

$$\mathbf{R}^{\text{trim}} = [\mathbf{R}^e \ \mathbf{R}_a^{\text{ie}}]^T = \mathbf{J}^{\text{trim}} - \bar{\mathbf{J}}^{\text{trim}} = \mathbf{0}$$

Augmented Lagrangian functions

The adjoint-based optimization is equivalent to searching for the stationary point of the augmented Lagrangian function,

$$\mathcal{L}(\mathbf{U}, \mathbf{x}, \boldsymbol{\lambda}, \boldsymbol{\mu}) = J^{\text{adapt}}(\mathbf{U}, \mathbf{x}) + \boldsymbol{\lambda}^T \mathbf{R}(\mathbf{U}, \mathbf{x}) + \boldsymbol{\mu}^T \mathbf{R}^{\text{trim}}(\mathbf{U}, \mathbf{x})$$

where $\boldsymbol{\lambda}$ and $\boldsymbol{\mu}$ are Lagrange multipliers associated with the flow equations and the trim constraints, respectively



Optimality Condition

- First-order optimality (Karush-Kuhn-Tucker) condition

$$\frac{\partial \mathcal{L}}{\partial \mathbf{x}} = \frac{\partial J^{\text{adapt}}}{\partial \mathbf{x}} + \boldsymbol{\lambda}^T \frac{\partial \mathbf{R}}{\partial \mathbf{x}} + \boldsymbol{\mu}^T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{x}} = \mathbf{0} \quad \text{optimal design}$$

$$\frac{\partial \mathcal{L}}{\partial \mathbf{U}} = \frac{\partial J^{\text{adapt}}}{\partial \mathbf{U}} + \boldsymbol{\lambda}^T \frac{\partial \mathbf{R}}{\partial \mathbf{U}} + \boldsymbol{\mu}^T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{U}} = \mathbf{0} \quad \text{coupled adjoint}$$

$$\frac{\partial \mathcal{L}}{\partial \boldsymbol{\lambda}} = \mathbf{R}(\mathbf{U}, \mathbf{x}) = \mathbf{0} \quad \text{physics feasibility}$$

$$\frac{\partial \mathcal{L}}{\partial \boldsymbol{\mu}} = \mathbf{R}^{\text{trim}}(\mathbf{U}, \mathbf{x}) = \mathbf{0} \quad \text{trim condition}$$

- Always physically feasible: $\mathbf{R}(\mathbf{U}, \mathbf{x}) = \mathbf{0}$
- Choose coupled adjoints variables, such that,

$$\begin{aligned} \frac{\partial \mathcal{L}}{\partial \mathbf{U}} = \mathbf{0} &\Rightarrow \boldsymbol{\lambda}^T = - \left(\frac{\partial J^{\text{adapt}}}{\partial \mathbf{U}} + \boldsymbol{\mu}^T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{U}} \right) \frac{\partial \mathbf{R}}{\partial \mathbf{U}}^{-1} \\ &= (\boldsymbol{\Psi}^{\text{adapt}} + \boldsymbol{\Psi}^{\text{trim}} \boldsymbol{\mu})^T \end{aligned}$$



Reduced optimality condition

- Coupled adjoints: $\lambda^T = (\Psi^{\text{adapt}} + \Psi^{\text{trim}} \mu)^T$, where

$$\frac{\partial \mathbf{R}^T}{\partial \mathbf{U}} \Psi^{\text{adapt}} + \frac{\partial J^{\text{adapt}^T}}{\partial \mathbf{U}} = \mathbf{0}, \quad \frac{\partial \mathbf{R}^T}{\partial \mathbf{U}} \Psi^{\text{trim}} + \frac{\partial \mathbf{J}^{\text{trim}^T}}{\partial \mathbf{U}} = \mathbf{0}$$

- Sensitivity Analysis

$$\begin{aligned} \frac{\partial \mathcal{L}}{\partial \mathbf{x}} &= \frac{\partial J^{\text{adapt}}}{\partial \mathbf{x}} + \lambda^T \frac{\partial \mathbf{R}}{\partial \mathbf{x}} + \mu^T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{x}} \\ &= \frac{\partial J^{\text{adapt}}}{\partial \mathbf{x}} + (\Psi^{\text{adapt}})^T \frac{\partial \mathbf{R}}{\partial \mathbf{x}} + \mu^T \left[\frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{x}} + (\Psi^{\text{trim}})^T \frac{\partial \mathbf{R}}{\partial \mathbf{x}} \right] \\ &= \frac{dJ^{\text{adapt}}}{d\mathbf{x}} + \mu^T \frac{d\mathbf{J}^{\text{trim}}}{d\mathbf{x}} \end{aligned}$$

- Reduced optimality condition:

$$\begin{aligned} \frac{\partial \mathcal{L}}{\partial \mathbf{x}} &= \frac{dJ^{\text{adapt}}}{d\mathbf{x}} + \mu^T \frac{d\mathbf{J}^{\text{trim}}}{d\mathbf{x}} = \mathbf{0} \\ \frac{\partial \mathcal{L}}{\partial \mu} &= \mathbf{R}^{\text{trim}} = \mathbf{0} \end{aligned}$$



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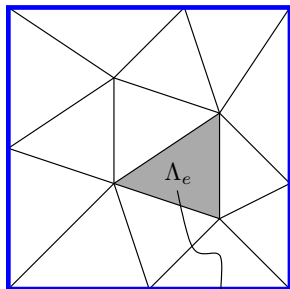
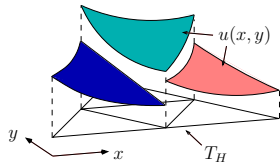
Discretization

- Conservation law: $\partial_t \mathbf{u} + \nabla \cdot \vec{\mathbf{H}}(\mathbf{u}, \nabla \mathbf{u}) = \mathbf{0}$

$$\text{where } \underbrace{\vec{\mathbf{H}}}_{\text{total flux}} = \underbrace{\vec{\mathbf{F}}(\mathbf{u})}_{\text{inviscid flux}} + \underbrace{\vec{\mathbf{G}}(\mathbf{u}, \nabla \mathbf{u})}_{\text{viscous flux}}$$

- DG approx of order p_e on each element:

$$\mathbf{u}_h(\vec{x}) = \sum_{e=1}^{N_e} \sum_{n=1}^{N_p} \mathbf{U}_{e,n} \phi_{e,n}(\vec{x})$$



domain Λ

element e

N_e = # of elements

p_e = approx order on element e

N_{p_e} = # of basis fcn on element e

$\phi_{e,n}(\vec{x})$ = n^{th} basis fcn of order p_e on e

$\mathbf{U}_{e,n}$ = coefficients vector of n^{th} basis function on element e



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Output-Based Error Estimation

For a given configuration (design) \mathbf{x} , the outputs (objective and constraints) are based on a **pure** CFD flow solve.

Output Error: $\delta J = J_H(\mathbf{U}_H, \mathbf{x}) - J(\mathbf{U}, \mathbf{x})$

This is the difference between J computed with the discrete system solution, \mathbf{U}_H , and J computed with the *exact* solution, \mathbf{U} .

Error Surrogate: $\delta J = J_H(\mathbf{U}_H, \mathbf{x}) - J_h(\mathbf{U}_h, \mathbf{x})$

The difference between outputs on coarse and fine discretizations.

$$\text{coarse space: } \rightarrow \underbrace{\mathbf{R}_H(\mathbf{U}_H, \mathbf{x}) = \mathbf{0}}_{N_H \text{ flow equations}} \rightarrow \underbrace{\mathbf{U}_H}_{\text{state} \in \mathbb{R}^{N_H}} \rightarrow J_H(\mathbf{U}_H, \mathbf{x})$$

$$\text{fine space: } \rightarrow \underbrace{\mathbf{R}_h(\mathbf{U}_h, \mathbf{x}) = \mathbf{0}}_{N_h \text{ flow equations}} \rightarrow \underbrace{\mathbf{U}_h}_{\text{state} \in \mathbb{R}^{N_h}} \rightarrow J_h(\mathbf{U}_h, \mathbf{x})$$



Adjoint-based Error Estimation

- State injection: $\mathbf{U}_h^H = \mathbf{I}_h^H \mathbf{U}_H$
- \mathbf{U}_h^H will generally not satisfy the fine-space equations,

$$\mathbf{R}_h(\mathbf{U}_h^H, \mathbf{x}) \neq \mathbf{0}$$

- Recall the definition of the output adjoint, $\frac{\partial \mathbf{R}}{\partial \mathbf{U}}^T \boldsymbol{\Psi} + \frac{\partial J}{\partial \mathbf{U}}^T = \mathbf{0}$. $\boldsymbol{\Psi}$ relates the residual perturbation to an output perturbation,

$$\delta J = \underbrace{\frac{\partial J}{\partial \mathbf{U}} \delta \mathbf{U}}_{\text{adjoint definition}} = \underbrace{-\boldsymbol{\Psi}^T \frac{\partial \mathbf{R}}{\partial \mathbf{U}} \delta \mathbf{U}}_{\text{residual linearization}} \approx -\boldsymbol{\Psi}^T \delta \mathbf{R}$$

$$\begin{aligned} \delta J &= J_H(\mathbf{U}_H, \mathbf{x}) - J_h(\mathbf{U}_h, \mathbf{x}) = J_h(\mathbf{U}_h^H, \mathbf{x}) - J_h(\mathbf{U}_h, \mathbf{x}) \\ &\approx -\boldsymbol{\Psi}_h^T \delta \mathbf{R}_h = -\boldsymbol{\Psi}_h^T \mathbf{R}_h(\mathbf{U}_h^H, \mathbf{x}) \end{aligned}$$

- Error (Adapt) indicator: the error is localized in each element and serves as an adaptation indicator, $\eta_e = |\boldsymbol{\Psi}_{h,e}^T \mathbf{R}_{h,e}(\mathbf{U}_h^H, \mathbf{x})|$



Error Estimation and Mesh Adaptation for Optimization

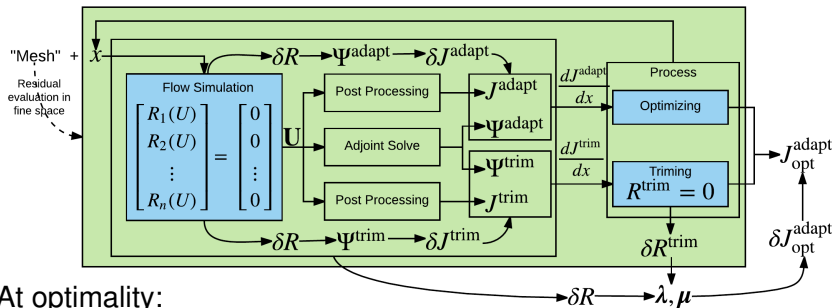
- Numerical error affects both objective and constraint outputs.
- How to estimate the error and adapt the mesh efficiently?
- Both errors can be obtained via adjoints.
- Possible adaptation strategies:
 - 1 Adapt only on the objective
Error due to inexact constraints satisfaction
 - 2 Adapt equally on the objective and constraints
Inefficient, expensive to keep all outputs very accurate
 - 3 Adapt on combined/weighted outputs
The weights? Adapt more on objective/constraints?
 - 4 Adapt on the optimization problem (coupled adjoint)

coarse space: $\mathbf{x}_0 \rightarrow \text{optimization} \rightarrow \underbrace{\mathbf{x}_H^*, \mathbf{U}_H}_{\text{optimal design}} \rightarrow J_H(\mathbf{U}_H, \mathbf{x}_H^*)$

fine space: $\mathbf{x}_0 \rightarrow \text{optimization} \rightarrow \underbrace{\mathbf{x}_h^*, \mathbf{U}_h}_{\text{optimal design}} \rightarrow J_h(\mathbf{U}_h, \mathbf{x}_h^*)$



Error Estimation and Mesh Adaptation for Optimization



$$\frac{\partial \mathcal{L}}{\partial \mathbf{x}} = \frac{\partial J^{\text{adapt}}}{\partial \mathbf{x}} + \lambda^T \frac{\partial \mathbf{R}}{\partial \mathbf{x}} + \mu^T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{x}} = \mathbf{0}$$

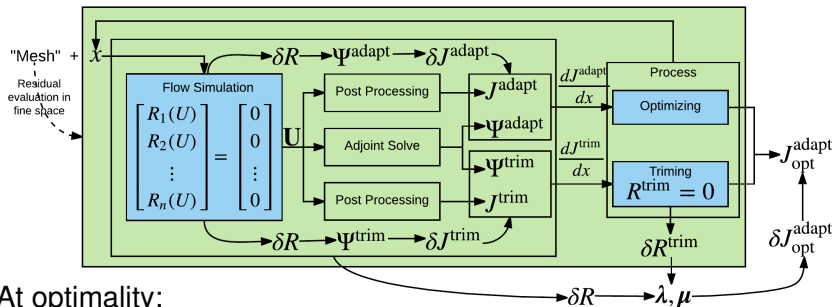
$$\frac{\partial \mathcal{L}}{\partial \mathbf{U}} = \frac{\partial J^{\text{adapt}}}{\partial \mathbf{U}} + \lambda^T \frac{\partial \mathbf{R}}{\partial \mathbf{U}} + \mu^T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{U}} = \mathbf{0}$$

$$\frac{\partial \mathcal{L}}{\partial \lambda} = \mathbf{R}(\mathbf{U}, \mathbf{x}) = \mathbf{0}$$

$$\frac{\partial \mathcal{L}}{\partial \mu} = \mathbf{R}^{\text{trim}}(\mathbf{U}, \mathbf{x}) = \mathbf{0}$$



Error Estimation and Mesh Adaptation for Optimization



At optimality:

$$\begin{aligned}
 \delta J_{\text{opt}}^{\text{adapt}} &= -\lambda_h^T \delta \mathbf{R}_h - \mu_h^T \delta \mathbf{R}_h^{\text{trim}} \\
 &= -\lambda_h^T \mathbf{R}_h(\mathbf{U}_h^H, \mathbf{x}_H) - \mu_h^T \mathbf{R}_h^{\text{trim}}(\mathbf{U}_h^H, \mathbf{x}_H) \\
 &= -(\Psi_h^{\text{adapt}} + \Psi_h^{\text{trim}} \mu_h)^T \mathbf{R}_h(\mathbf{U}_h^H, \mathbf{x}_H) - \mu_h^T \underbrace{(\mathbf{J}_h^{\text{trim}}(\mathbf{U}_h^H, \mathbf{x}_H) - \bar{\mathbf{J}}^{\text{trim}})}_{\approx 0} \\
 &= \delta J^{\text{adapt}}(\mathbf{x}_H) + \mu_h^T \delta \mathbf{J}^{\text{trim}}(\mathbf{x}_H)
 \end{aligned}$$

Note: $\mathbf{J}_h^{\text{trim}}(\mathbf{U}_h^H, \mathbf{x}_H) = \mathbf{J}_H^{\text{trim}}(\mathbf{U}_H, \mathbf{x}_H) = \bar{\mathbf{J}}^{\text{trim}} = \mathbf{J}_h^{\text{trim}}(\mathbf{U}_h, \mathbf{x}_h)$



Optimality error estimation

$$\frac{dJ^{\text{adapt}}}{d\mathbf{x}} + \boldsymbol{\mu}^T \frac{d\mathbf{J}^{\text{trim}}}{d\mathbf{x}} = \mathbf{0}$$
$$\delta J_{\text{opt}}^{\text{adapt}} = \underbrace{\delta J^{\text{adapt}}(\mathbf{x}_H)}_{\text{objective error only}} + \underbrace{\boldsymbol{\mu}_h^T \delta \mathbf{J}^{\text{trim}}(\mathbf{x}_H)}_{\text{inexact constraints satisfaction}}$$

What does $\boldsymbol{\mu}$ mean?

It is the objective sensitivity w.r.t constraints and measures how much the constraints error can affect the optimal objective.

Mesh adaptation implementation

Adapt (error) indicator: $\eta_{\kappa} = |\boldsymbol{\Psi}_{h,\kappa}^T \mathbf{R}_{h,\kappa}(\mathbf{U}_h^H, \mathbf{x}_H)|$

Combined indicator: $\eta_{\kappa,\text{opt}} = \eta_{\kappa}^{\text{adapt}} + |\boldsymbol{\mu}|^T \boldsymbol{\eta}_{\kappa}^{\text{trim}}$

$\boldsymbol{\Psi}_h$: reconstructing the coarse-space adjoints $\boldsymbol{\Psi}_H$

$\boldsymbol{\mu}_h$: extracted from the optimizer on the coarse space



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Multi-fidelity Optimization with Error Control

Geometry and Mesh

- Airfoil parameterization: Hicks-Henne basis function
- Design parameters: airfoil shape + angle of attack
- Mesh movement: Radial Basis Function (RBF) interpolation

Optimization Algorithm

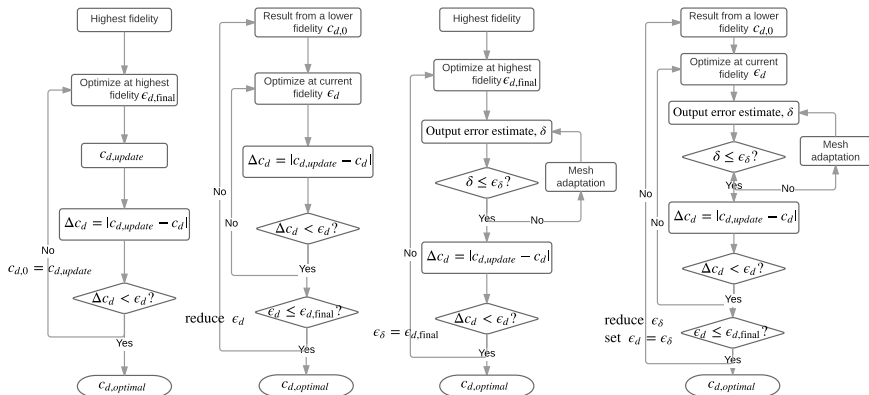
- Sequential Least Squares Programming (SLSQP)
- Broyden-Fletcher-Goldfarb-Shanno (BFGS) Hessian update
- Inexact line search: weak Wolfe condition



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Laminar, Subsonic Flow (nearly feasible starting point)

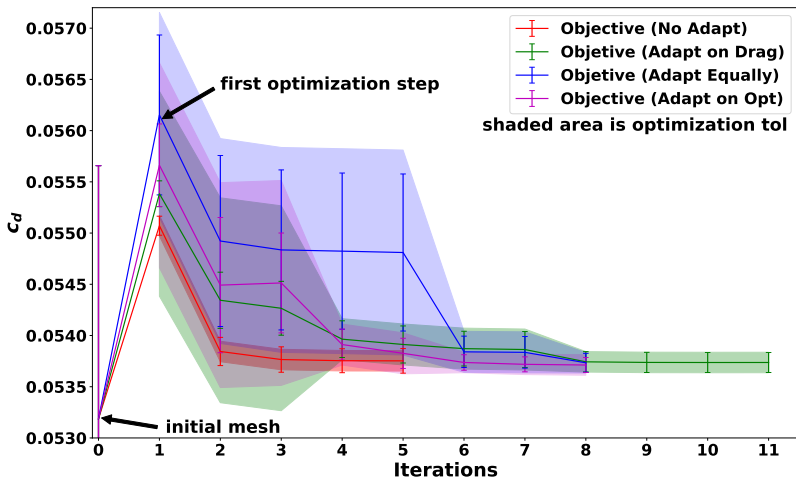
$$\text{NACA 0012, } Re = 5000, M_\infty = 0.5, \alpha_0 = 0^\circ$$
$$J^{\text{adapt}} = c_d, J^{\text{trim}} = c_l, \bar{J}^{\text{trim}} = 0.02, A \geq A_{\min}$$



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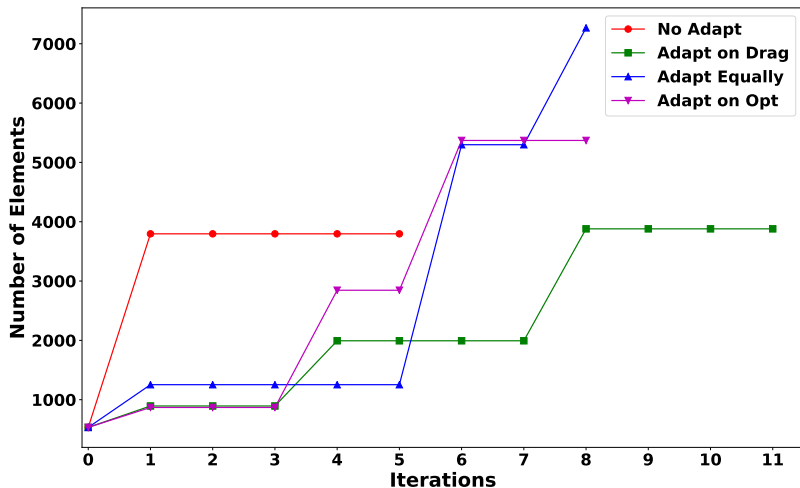
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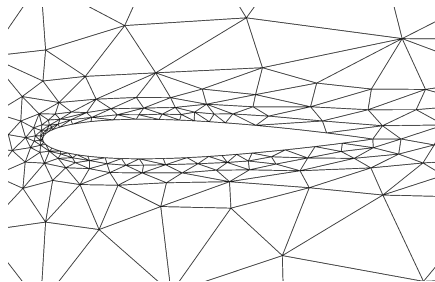


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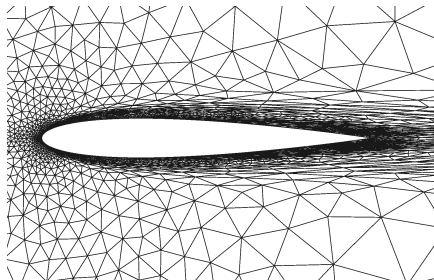


Mesh Evolution



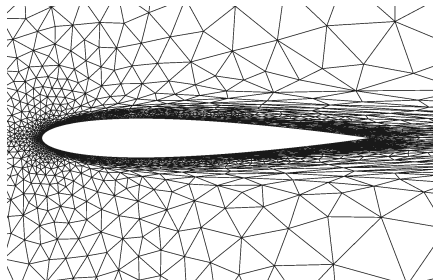
initial mesh (533 elements)

Mesh Evolution

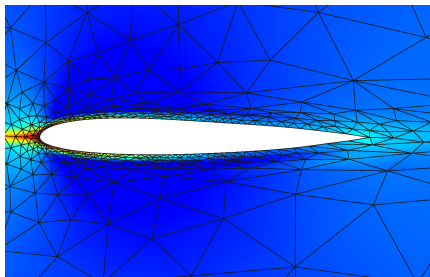


no adapt (3796 elements)

Mesh Evolution

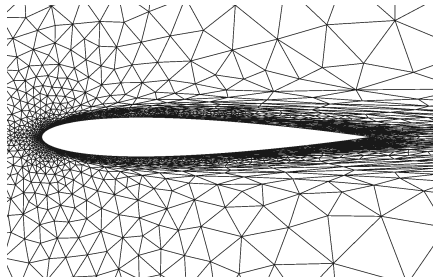


no adapt (3796 elements)

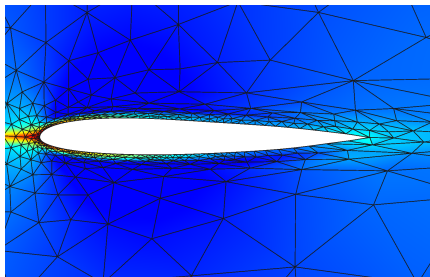


drag adapt (894 elems, Ψ^{adapt})

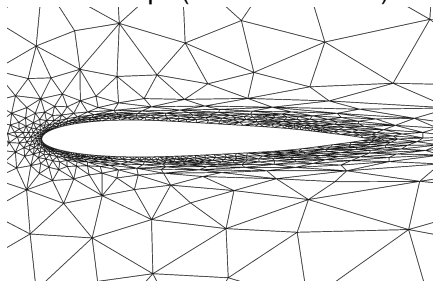
Mesh Evolution



no adapt (3796 elements)



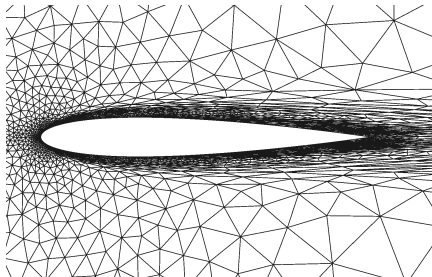
drag adapt (894 elems, Ψ^{adapt})



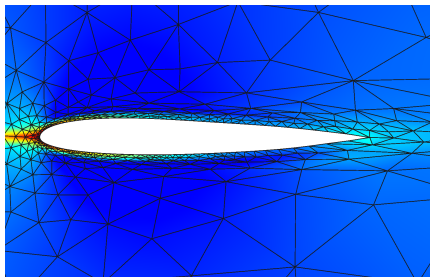
adapt equally (1253 elements)



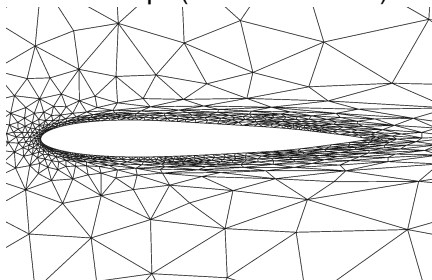
Mesh Evolution



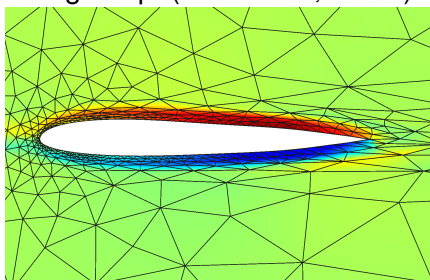
no adapt (3796 elements)



drag adapt (894 elems, Ψ^{adapt})

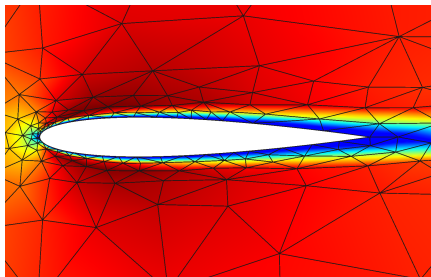


adapt equally (1253 elements)



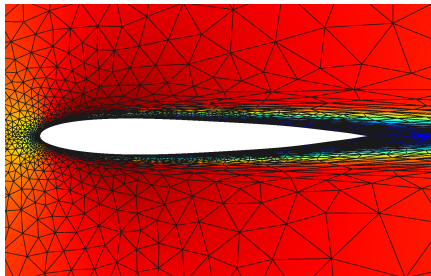
opt adapt (869 elems, Ψ^{trim})

Optimized design (Mach Contour 0 ~ 0.6)



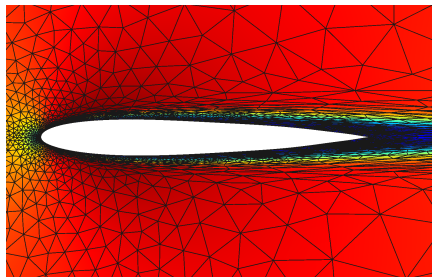
initial airfoil ($\alpha = 0^\circ$)

Optimized design (Mach Contour 0 ~ 0.6)

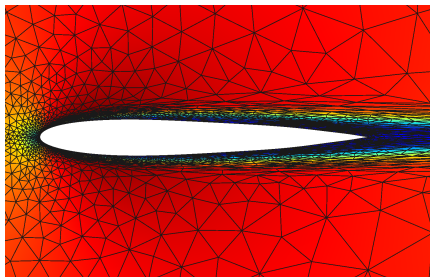


no adapt ($\alpha = 0.27^\circ$)

Optimized design (Mach Contour 0 ~ 0.6)

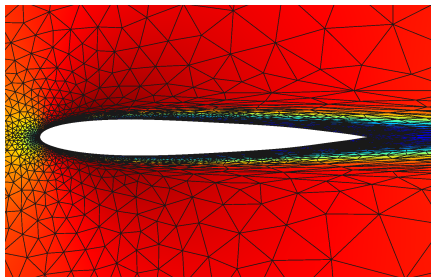


no adapt ($\alpha = 0.27^\circ$)

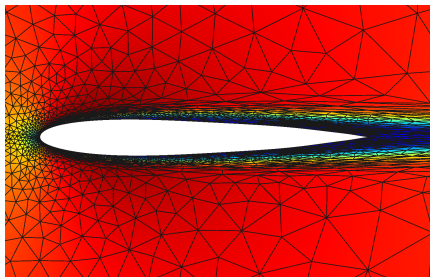


adapt on drag ($\alpha = 0.30^\circ$)

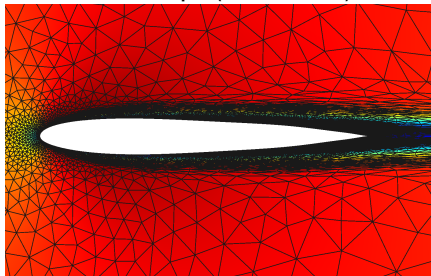
Optimized design (Mach Contour 0 ~ 0.6)



no adapt ($\alpha = 0.27^\circ$)



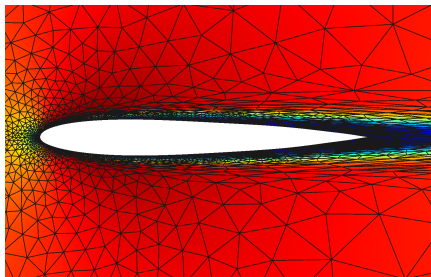
adapt on drag ($\alpha = 0.30^\circ$)



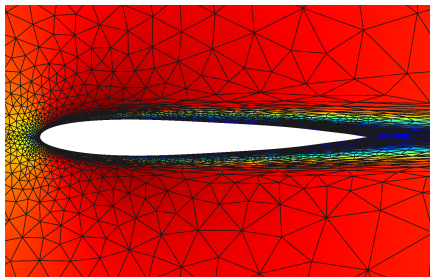
adapt equally ($\alpha = 0.25^\circ$)



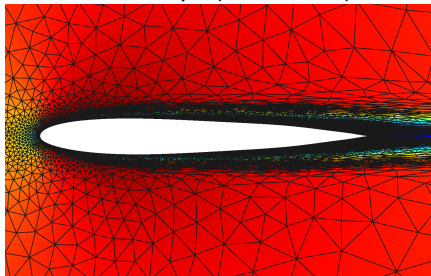
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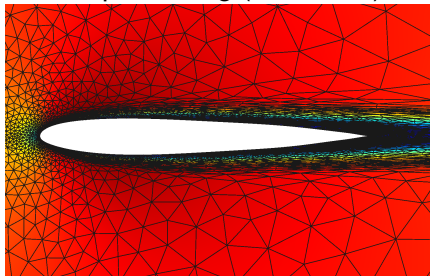
no adapt ($\alpha = 0.27^\circ$)



adapt on drag ($\alpha = 0.30^\circ$)



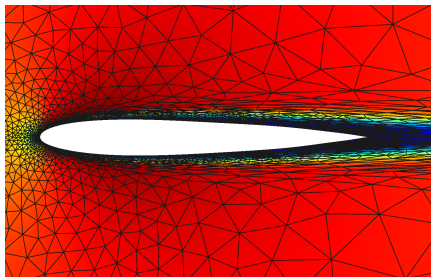
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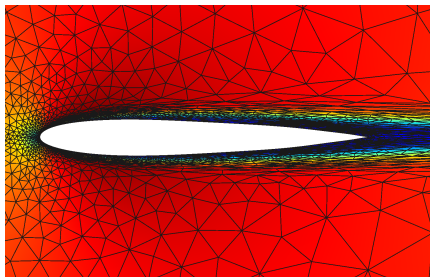
adapt on opt ($\alpha = 0.24^\circ$)



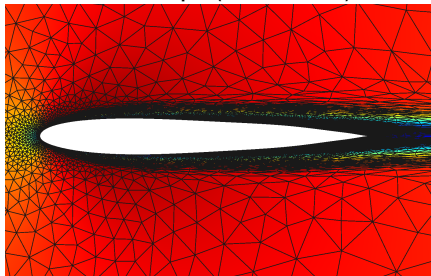
Optimized design (Mach Contour 0 ~ 0.6)



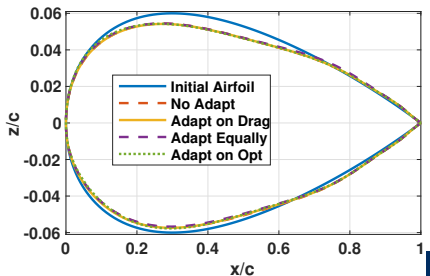
no adapt ($\alpha = 0.27^\circ$)



adapt on drag ($\alpha = 0.30^\circ$)



adapt equally ($\alpha = 0.25^\circ$)



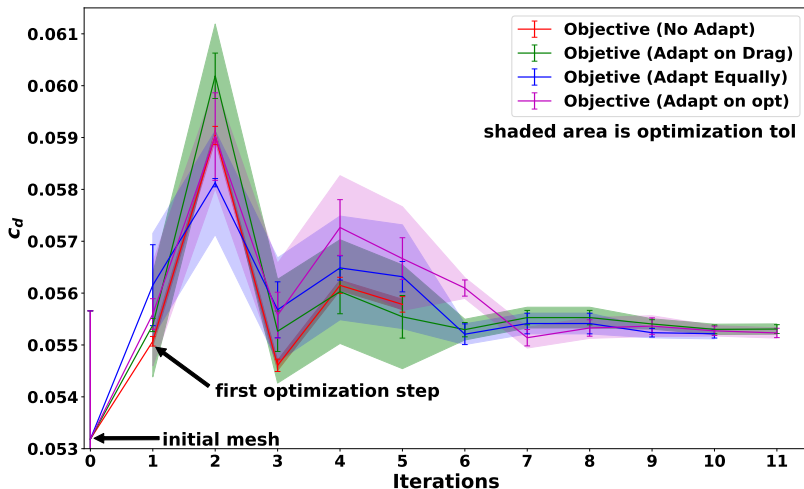
final design



Laminar, Subsonic Flow (infeasible starting point)

NACA 0012, $Re = 5000$, $M_\infty = 0.5$, $\alpha_0 = 0^\circ$

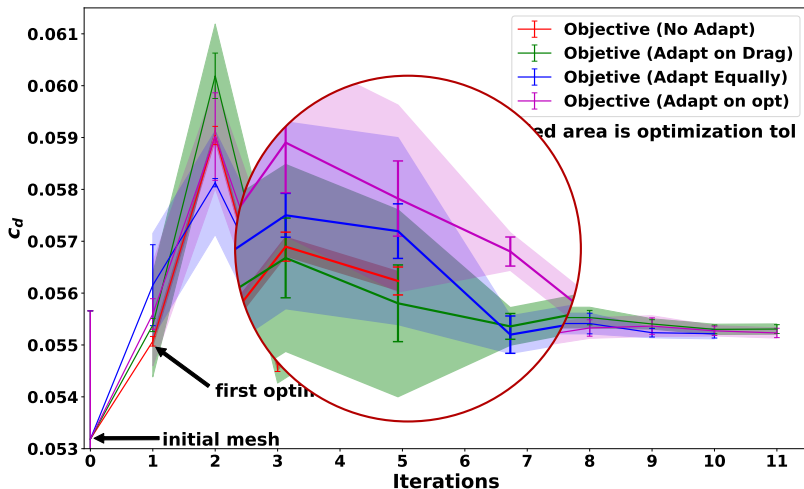
$$J^{\text{adapt}} = c_d, J^{\text{trim}} = c_l, \bar{J}^{\text{trim}} = 0.1, A \geq A_{\min}$$



Laminar, Subsonic Flow (infeasible starting point)

NACA 0012, $Re = 5000$, $M_\infty = 0.5$, $\alpha_0 = 0^\circ$

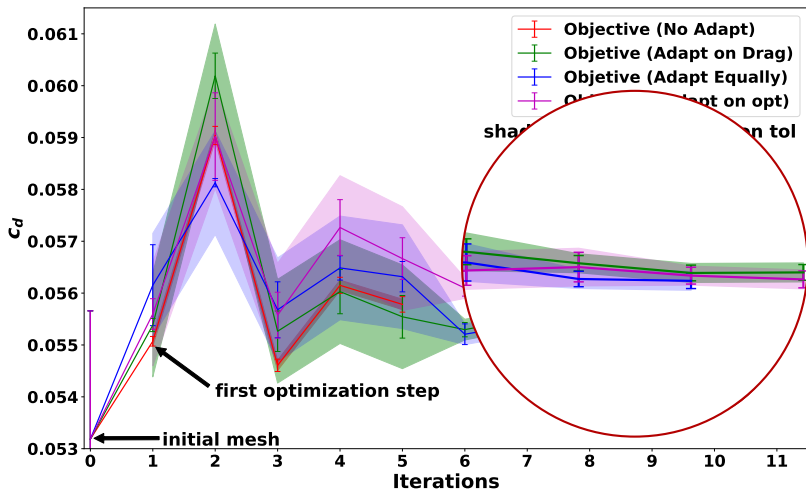
$$J^{\text{adapt}} = c_d, J^{\text{trim}} = c_l, \bar{J}^{\text{trim}} = 0.1, A \geq A_{\min}$$



Laminar, Subsonic Flow (infeasible starting point)

NACA 0012, $Re = 5000$, $M_\infty = 0.5$, $\alpha_0 = 0^\circ$

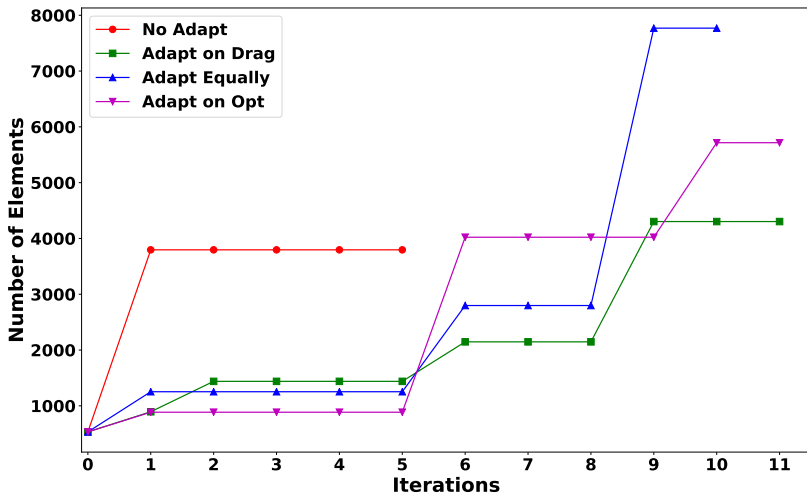
$J^{\text{adapt}} = c_d$, $J^{\text{trim}} = c_l$, $\bar{J}^{\text{trim}} = 0.1$, $A \geq A_{\min}$



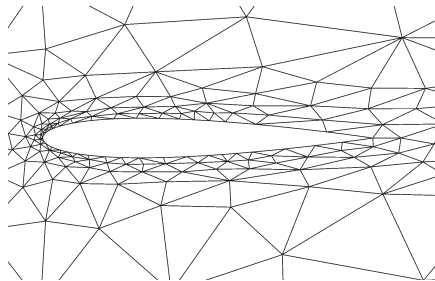
Laminar, Subsonic Flow (infeasible starting point)

NACA 0012, $Re = 5000$, $M_\infty = 0.5$, $\alpha_0 = 0^\circ$

$$J^{\text{adapt}} = c_d, J^{\text{trim}} = c_l, \bar{J}^{\text{trim}} = 0.1, A \geq A_{\min}$$

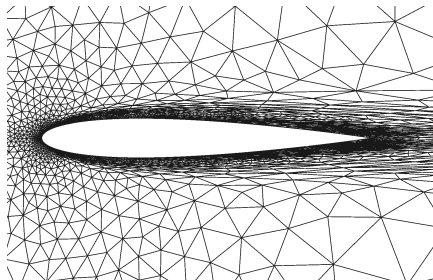


Mesh Evolution



initial mesh (533 elements)

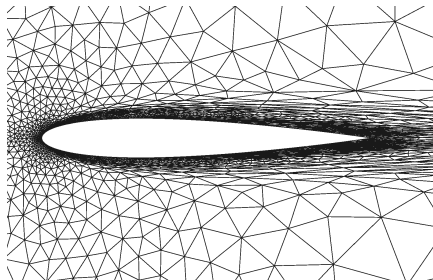
Mesh Evolution



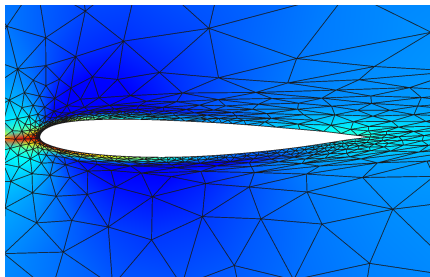
no adapt (3796 elements)



Mesh Evolution

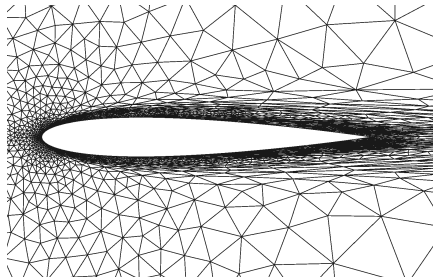


no adapt (3796 elements)

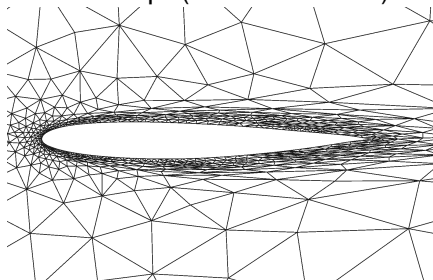


drag adapt (1439 elems, Ψ^{adapt})

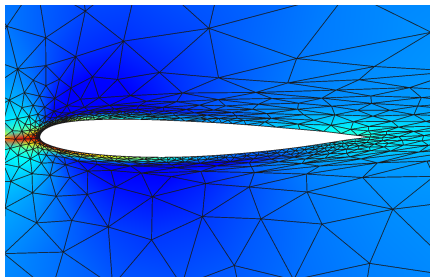
Mesh Evolution



no adapt (3796 elements)



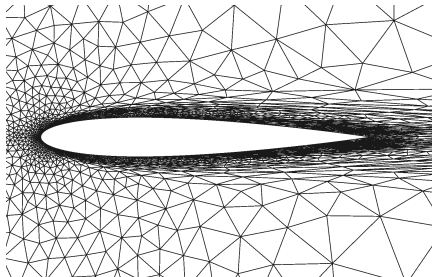
adapt equally (1253 elems)



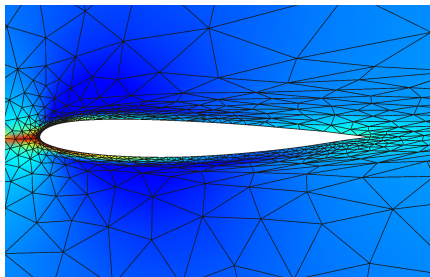
drag adapt (1439 elems, Ψ^{adapt})



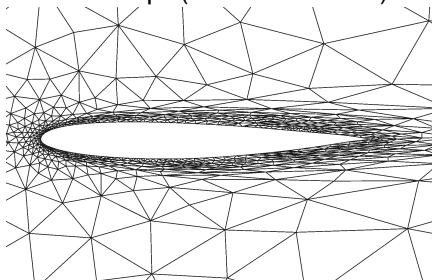
Mesh Evolution



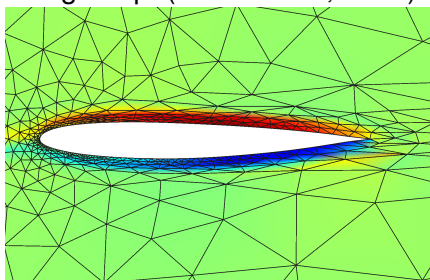
no adapt (3796 elements)



drag adapt (1439 elems, Ψ^{adapt})



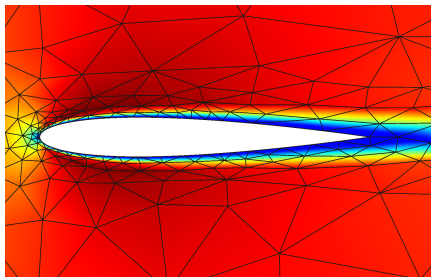
adapt equally (1253 elems)



opt adapt (886 elems, Ψ^{trim})

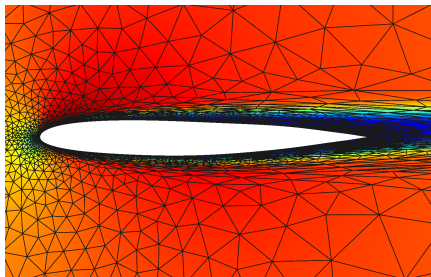


Optimized design (Mach Contour 0 ~ 0.6)



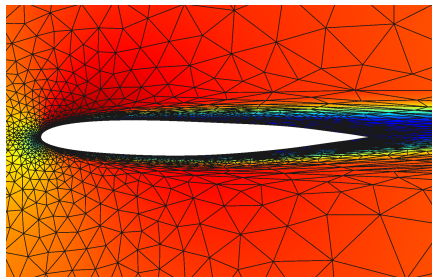
initial airfoil ($\alpha = 0^\circ$)

Optimized design (Mach Contour 0 ~ 0.6)

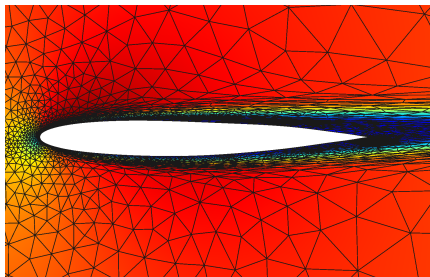


no adapt ($\alpha = 2.53^\circ$)

Optimized design (Mach Contour 0 ~ 0.6)

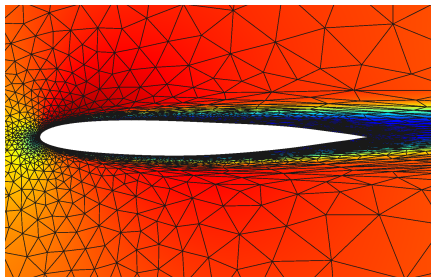


no adapt ($\alpha = 2.53^\circ$)

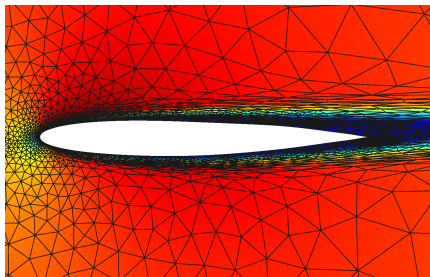


adapt on drag ($\alpha = 2.46^\circ$)

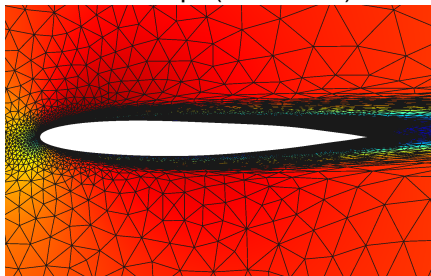
Optimized design (Mach Contour 0 ~ 0.6)



no adapt ($\alpha = 2.53^\circ$)



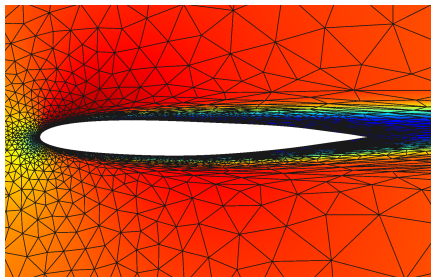
adapt on drag ($\alpha = 2.46^\circ$)



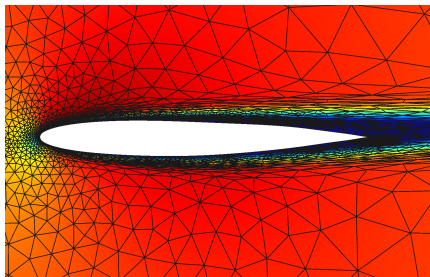
adapt equally ($\alpha = 2.39^\circ$)



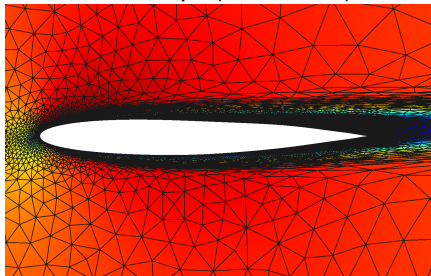
Optimized design (Mach Contour 0 ~ 0.6)



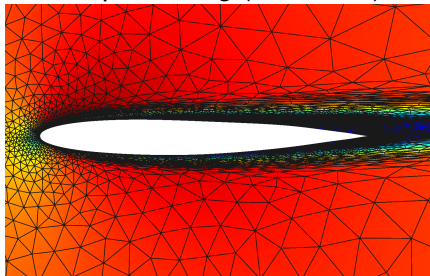
no adapt ($\alpha = 2.53^\circ$)



adapt on drag ($\alpha = 2.46^\circ$)



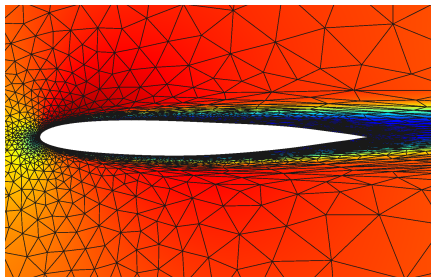
adapt equally ($\alpha = 2.39^\circ$)



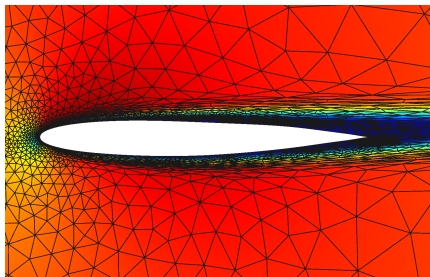
adapt on opt ($\alpha = 2.40^\circ$)



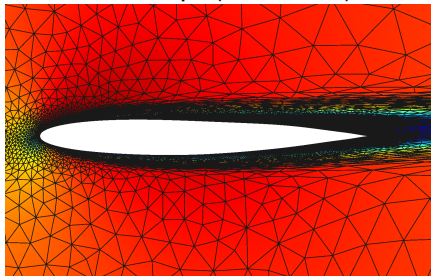
Optimized design (Mach Contour 0 ~ 0.6)



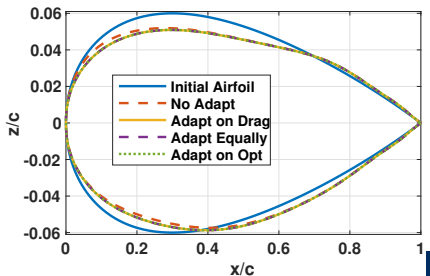
no adapt ($\alpha = 2.53^\circ$)



adapt on drag ($\alpha = 2.46^\circ$)



adapt equally ($\alpha = 2.39^\circ$)

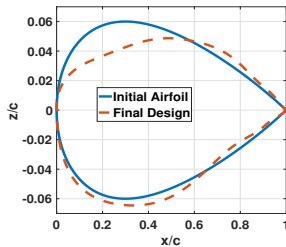
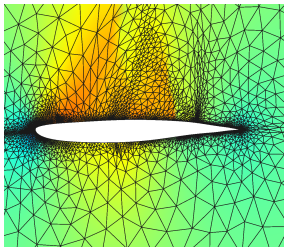
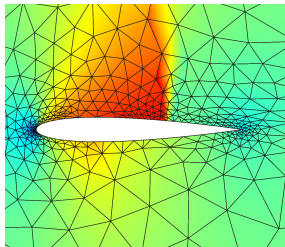
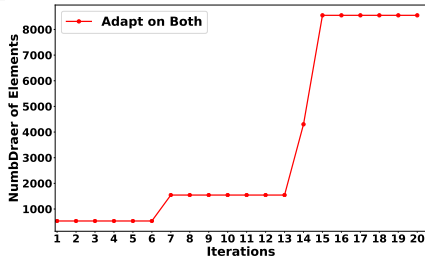
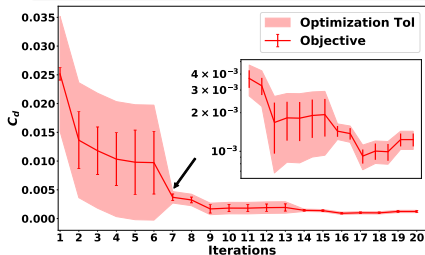


final design



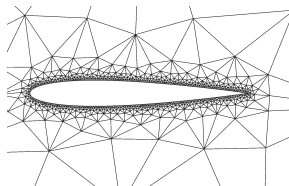
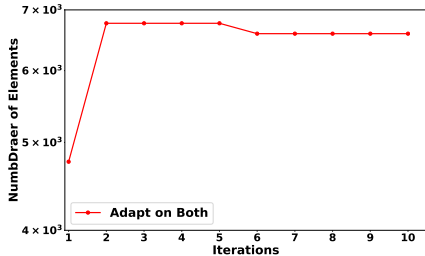
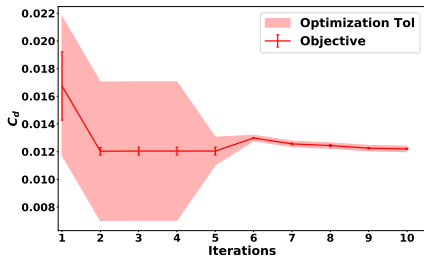
Inviscid, Transonic Flow

$$\text{NACA 0012, } M_\infty = 0.8, \alpha_0 = 1.25^\circ$$
$$J^{\text{adapt}} = c_d, J^{\text{trim}} = c_l, \bar{J}^{\text{trim}} = 0.4, A \geq A_{\text{min}}$$

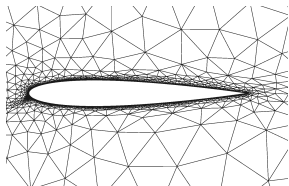


Turbulent, Low-Speed Flow

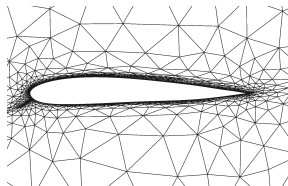
$$\text{NACA } 0012, Re = 10^6, M_\infty = 0.15, \alpha_0 = 6^\circ$$
$$J^{\text{adapt}} = c_d, J^{\text{trim}} = c_l, \bar{J}^{\text{trim}} = 0.6, A \geq A_{\min}$$



initial mesh



first step mesh

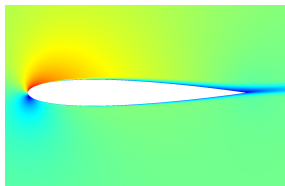
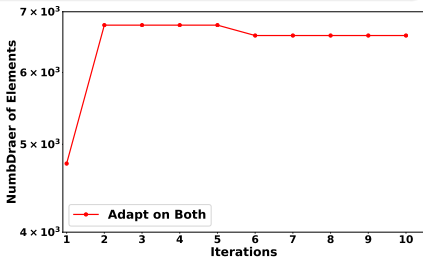
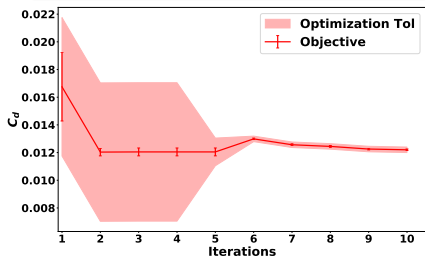


final mesh

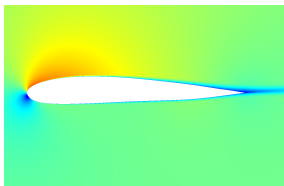


Turbulent, Low-Speed Flow

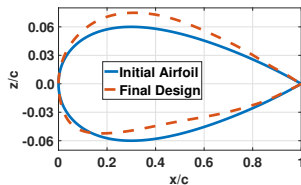
$$\text{NACA 0012, } Re = 10^6, M_\infty = 0.15, \alpha_0 = 6^\circ$$
$$J^{\text{adapt}} = c_d, J^{\text{trim}} = c_l, \bar{J}^{\text{trim}} = 0.6, A \geq A_{\min}$$



initial design



final design



airfoil shape

Outline

- 1 Introduction
- 2 Optimization Problem
- 3 Discretization
- 4 Error Estimation and Mesh Adaptation
- 5 Optimization Approach
- 6 Results and Discussion
- 7 Conclusions and Future Work**



Conclusions:

- Numerical error should be carefully controlled as the shape and mesh change during the optimization
- We integrate output-based error estimation and mesh adaptation with a traditional gradient-based algorithm
- Error tolerance serves as the optimization tolerance at each fidelity, fidelity increases through mesh adaptation.
- Coupled adjoint error estimation offers a more efficient way to adapt the mesh for constrained optimization problem
- Prevent over-refining and over-optimizing during optimization

Future Work:

- Develop improved and automated fidelity increase strategy
- Avoid overshoot refinement, allow more mesh redistribution and coarsening, optimize mesh during the optimization
- Combined with h - p refinement

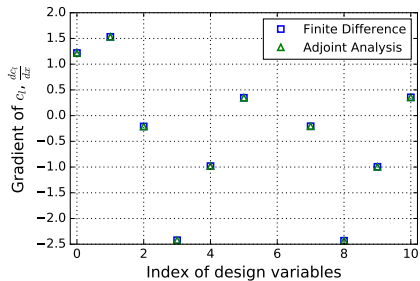
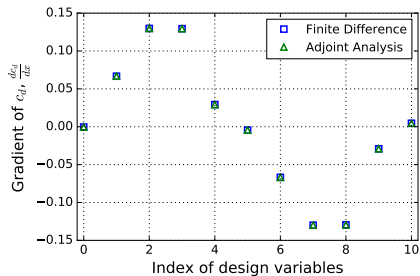


Acknowledgments

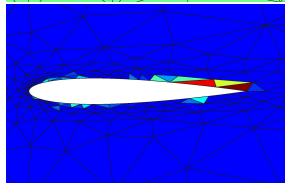
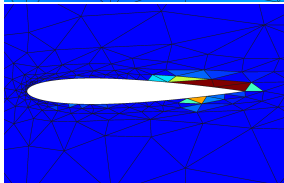
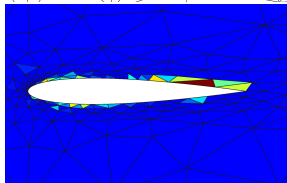
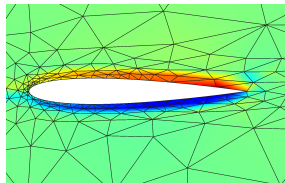
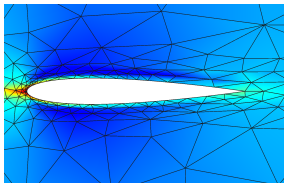
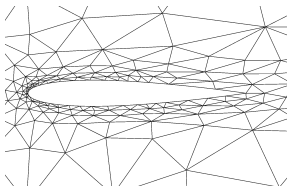
Department of Energy
DE-FG02-13ER26146/DE-SC0010341
Boeing Company, with technical monitor Dr. Mori Mani
— Thank you —



Sensitivity Verification



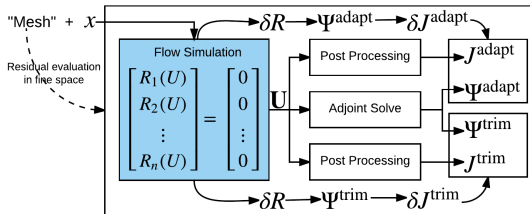
Adapt Indicator



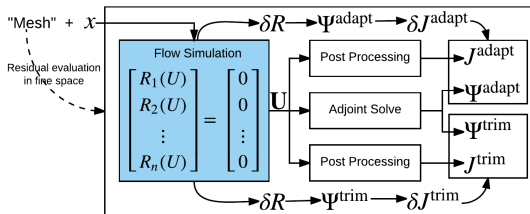
Complete Error Estimation



Error Estimation and Mesh Adaptation for Optimization



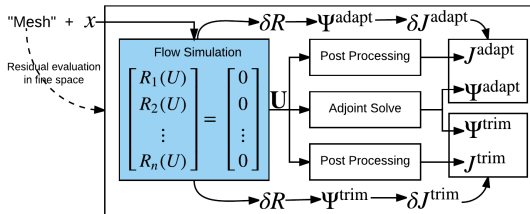
Error Estimation and Mesh Adaptation for Optimization



Flow problem:

$$\begin{aligned}\delta J &\approx J_h(\mathbf{U}_h^H, \mathbf{x}) - J_h(\mathbf{U}_h, \mathbf{x}) \\ &= -\Psi_h^T \delta \mathbf{R}_h \\ &= -\Psi_h^T \mathbf{R}_h(\mathbf{U}_h^H, \mathbf{x})\end{aligned}$$

Error Estimation and Mesh Adaptation for Optimization

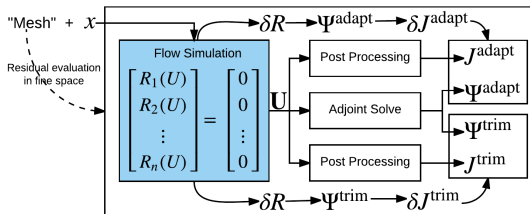


During optimization:

Flow problem:

$$\begin{aligned}
 \delta J &\approx J_h(\mathbf{U}_h^H, \mathbf{x}) - J_h(\mathbf{U}_h, \mathbf{x}) \\
 &= -\Psi_h^T \delta \mathbf{R}_h \\
 &= -\Psi_h^T \mathbf{R}_h(\mathbf{U}_h^H, \mathbf{x})
 \end{aligned}$$

Error Estimation and Mesh Adaptation for Optimization



Flow problem:

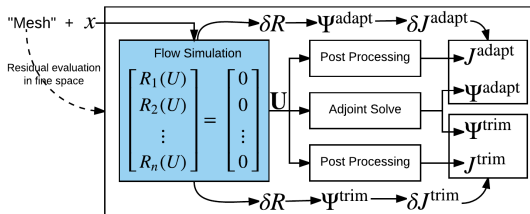
$$\begin{aligned}
 \delta J &\approx J_h(\mathbf{U}_h^H, \mathbf{x}) - J_h(\mathbf{U}_h, \mathbf{x}) \\
 &= -\Psi_h^T \delta \mathbf{R}_h \\
 &= -\Psi_h^T \mathbf{R}_h(\mathbf{U}_h^H, \mathbf{x})
 \end{aligned}$$

During optimization:

$$\begin{aligned}
 \frac{\partial \mathcal{L}}{\partial \mathbf{x}} &= \frac{\partial J^{\text{adapt}}}{\partial \mathbf{x}} + \lambda^T \frac{\partial \mathbf{R}}{\partial \mathbf{x}} + \mu^T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{x}} \neq \mathbf{0} \\
 \frac{\partial \mathcal{L}}{\partial \mathbf{U}} &= \frac{\partial J^{\text{adapt}}}{\partial \mathbf{U}} + \lambda^T \frac{\partial \mathbf{R}}{\partial \mathbf{U}} + \mu^T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{U}} = \mathbf{0} \\
 \frac{\partial \mathcal{L}}{\partial \lambda} &= \mathbf{R}(\mathbf{U}, \mathbf{x}) = \mathbf{0} \\
 \frac{\partial \mathcal{L}}{\partial \mu} &= \mathbf{R}^{\text{trim}}(\mathbf{U}, \mathbf{x}) \neq \mathbf{0}
 \end{aligned}$$



Error Estimation and Mesh Adaptation for Optimization



Flow problem:

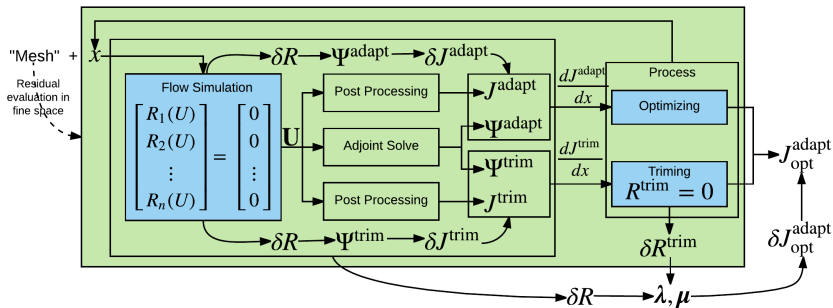
$$\begin{aligned} \delta J &\approx J_h(\mathbf{U}_h^H, \mathbf{x}) - J_h(\mathbf{U}_h, \mathbf{x}) \\ &= -\Psi_h^T \delta \mathbf{R}_h \\ &= -\Psi_h^T \mathbf{R}_h(\mathbf{U}_h^H, \mathbf{x}) \end{aligned}$$

During optimization:

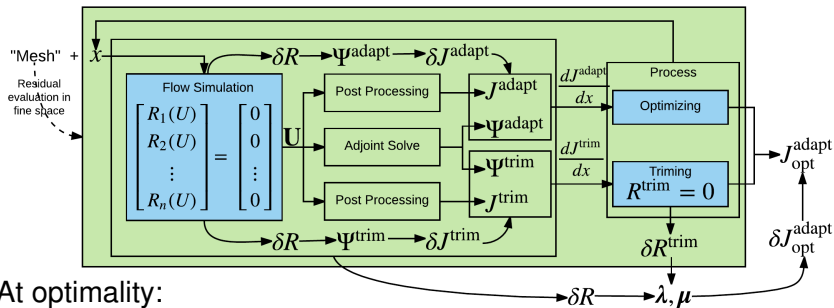
$$\begin{aligned} \delta J^{\text{adapt}} &= -\lambda_h^T \delta \mathbf{R}_h - \mu^T \delta \mathbf{R}_h^{\text{trim}} \\ &= -\lambda^T \mathbf{R}_h(\mathbf{U}_h^H, \mathbf{x}) - \mu^T \mathbf{R}_h^{\text{trim}}(\mathbf{U}_h^H, \mathbf{x}) \\ &= -(\Psi_h^{\text{adapt}} + \Psi_h \mu_h)^T \mathbf{R}_h(\mathbf{U}_h^H, \mathbf{x}) - \mu_h^T (J_h^{\text{trim}}(\mathbf{U}_h^H, \mathbf{x}) - J_h^{\text{trim}}(\mathbf{U}_h, \mathbf{x})) \\ &= \delta J^{\text{adapt}} + \underbrace{\mu_h^T (-\Psi_h^{\text{trim}})^T \mathbf{R}_h(\mathbf{U}_h^H, \mathbf{x})}_{\delta J^{\text{trim}}} - \mu_h^T \delta J^{\text{trim}} \\ &= \delta J^{\text{adapt}} \end{aligned}$$



Error Estimation and Mesh Adaptation for Optimization



Error Estimation and Mesh Adaptation for Optimization



At optimality:

$$\begin{aligned}
 \delta J^{\text{adapt}}_{\text{opt}} &= -\lambda_h^T \delta \mathbf{R}_h - \mu^T \delta \mathbf{R}_h^{\text{trim}} \\
 &= -\lambda^T \mathbf{R}_h(\mathbf{U}_h^H, \mathbf{x}_H) - \mu^T \mathbf{R}_h^{\text{trim}}(\mathbf{U}_h^H, \mathbf{x}_H) \\
 &= -(\Psi_h^{\text{adapt}} + \Psi_h \mu_h)^T \mathbf{R}_h(\mathbf{U}_h^H, \mathbf{x}_H) - \underbrace{\mu_h^T (J_h^{\text{trim}}(\mathbf{U}_h^H, \mathbf{x}_H) - \bar{J}^{\text{trim}})}_{\approx 0} \\
 &= \delta J^{\text{adapt}}(\mathbf{x}_H) + \mu_h^T \delta J^{\text{trim}}(\mathbf{x}_H)
 \end{aligned}$$

Note: $J_h^{\text{trim}}(\mathbf{U}_h^H, \mathbf{x}_H) = J_H^{\text{trim}}(\mathbf{U}_H, \mathbf{x}_H) = \bar{J}^{\text{trim}} = J_h^{\text{trim}}(\mathbf{U}_h, \mathbf{x}_h)$



Optimality error estimation

$$\frac{dJ^{\text{adapt}}}{d\mathbf{x}} + \boldsymbol{\mu}^T \frac{d\mathbf{J}^{\text{trim}}}{d\mathbf{x}} = \mathbf{0}$$
$$\delta J_{\text{opt}}^{\text{adapt}} = \delta J^{\text{adapt}}(\mathbf{x}_H) + \boldsymbol{\mu}_h^T \delta J^{\text{trim}}(\mathbf{x}_H)$$

What does $\boldsymbol{\mu}$ mean?

It is the objective sensitivity w.r.t constraints and measures how much the constraints error can affect the optimal objective.

Mesh adaptation implementation

Adapt (error) indicator: $\eta_{\kappa} = |\boldsymbol{\Psi}_{h,\kappa}^T \mathbf{R}_{h,\kappa}(\mathbf{U}_h^H, \mathbf{x}_H)|$

Combined indicator: $\eta_{\kappa,\text{opt}} = \underbrace{\eta_{\kappa}^{\text{adapt}}}_{\text{objective error only}} + \underbrace{|\boldsymbol{\mu}|^T \eta_{\kappa}^{\text{trim}}}_{\text{inexact constraints satisfaction}}$

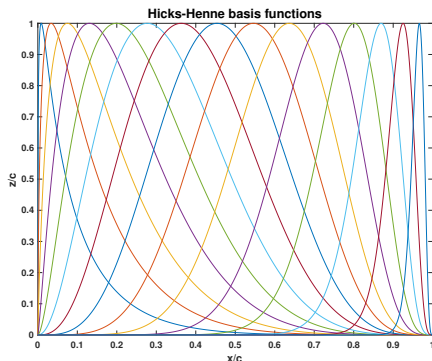
$\boldsymbol{\Psi}_h$: reconstructing the coarse-space adjoints $\boldsymbol{\Psi}_H$

$\boldsymbol{\mu}_h$: extracted from the optimizer on the coarse space



Airfoil Parameterization

- Hicks-Henne basis functions: linear combination of "bump" functions added to the baseline airfoil



$$z = z_{\text{base}} + \sum_{i=0}^n a_i \phi_i(x)$$

$$\phi_i(x) = \sin^{t_i}(\pi x^{m_i})$$

$$m_i = \ln(0.5) / \ln(x_{M_i})$$

x : coord along the airfoil chord

z : vertical surface coord

x_{M_i} : maxima location

t_i : width of the bump function

- Design parameters: $\mathbf{x} = [\alpha, a_1, a_2, \dots, a_n]^T$
Coefficients of Hicks-Henne basis + angle of attack α

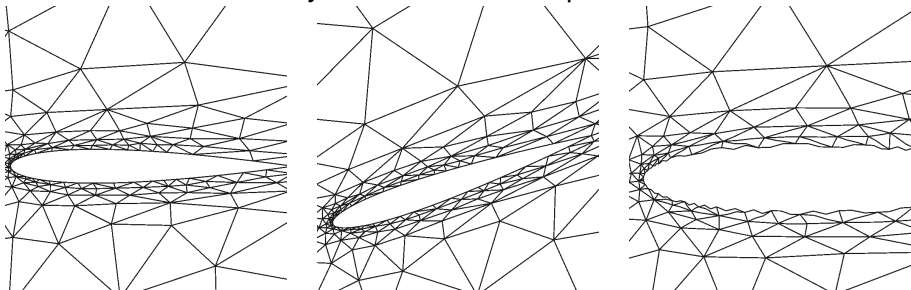


Mesh Movement

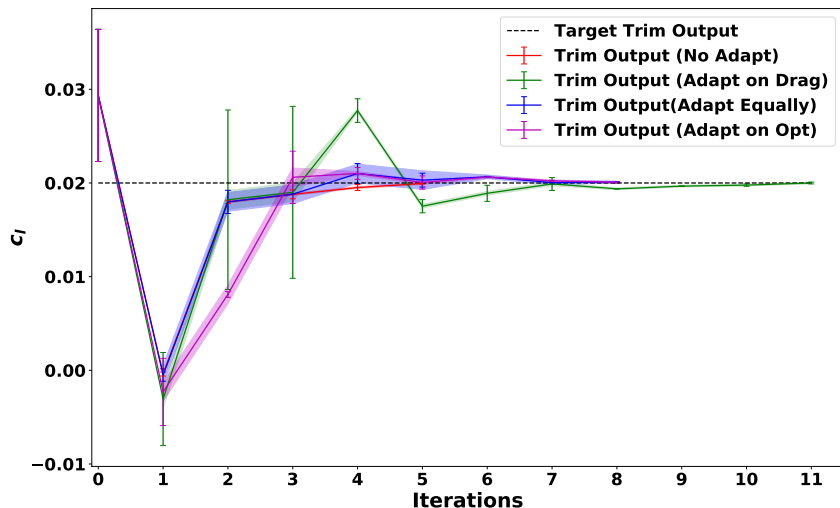
- Radial Basis Function (RBF): only depends on the distance from the origin or a center, e.g. $\phi(x) = e^{-x^2}$
- We can use a sum of RBFs $\phi(\|\vec{x}\|)$ and a polynomial $p(\vec{x})$ to interpolate the original function (mesh movement):

$$\vec{d}(\vec{x}) \approx \tilde{d}(\vec{x}) = \sum_{i=1}^{N_b} \vec{r}_i \phi(\|\vec{x} - \vec{x}_i\|) + \vec{p}(\vec{x})$$

- Solving for a linear system $\mathcal{O}(N_b)$ of \vec{r}_i
- Mesh connectivity information not required



Constraints, Nearly Feasible Starting Point



Constraints, Infeasible Starting Point

